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(72) Inventors:  
• **UEDA, Toshiyuki c/o TOYO KOHAN CO., LTD.**  
**Kudamatsu-shi, Yamaguchi 744-8611 (JP)**  
• **Yabuta, Naomi c/o TOYO KOHAN CO., LTD.**  
**Kudamatsu-shi, Yamaguchi 744-8611 (JP)**  
• **Aoki, Shinichi c/o TOYO KOHAN CO., LTD.**  
**Kudamatsu-shi, Yamaguchi 744-8611 (JP)**

(30) Priority: **21.11.2000 JP 2000354284**

(71) Applicant: **Toyo Kohan Co., Ltd.**  
**Tokyo 102-8447 (JP)**

(74) Representative: **VOSSIUS & PARTNER**  
**Siebertstrasse 4**  
**81675 München (DE)**

(54) **MATERIAL FOR SHADOW MASK, METHOD FOR PRODUCTION THEREOF, SHADOW MASK  
COMPRISING THE MATERIAL AND PICTURE TUBE USING THE SHADOW MASK**

(57) A material for a shadow mask, characterized in that it has a chemical composition: C = 0.0030 wt%, Si = 0.03 wt%, Mn : 0.1 to 0.5 wt%, P = 0.02 wt%, S = 0.02 wt%, Al: 0.01 to 0.07 wt%, N = 0.0030 wt%, B: an amount satisfying  $0.5 \leq B/N \leq 2$ , and balance: Fe and inevitable impurities, and can form a shadow mask having a coercive force H<sub>c</sub> of 90 A/m or less; and a method for producing the material, characterized in that use is made of a raw material having the above chemical com-

position, the finishing temperature in hot rolling is lower than Ar<sub>3</sub> point by 0 to 30 °C, the coiling temperature is 650 to 700 °C, and the rolling reduction percentage in the final rolling (secondary cold rolling) is 30 to 45 %. The material produced by the method exhibits magnetic characteristics being uniform in a coil and excellent as described above.

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**Description****TECHNICAL FIELD**

- 5    **[0001]** The present invention relates to a material for shadow masks to be in color picture tubes, a method for producing it, a shadow mask made of the material, and a picture tube comprising the shadow mask.

**BACKGROUND ART**

- 10   **[0002]** For the material for shadow masks, cold-rolled sheet steel has heretofore been produced according to a process mentioned below. Specifically, low-carbon steel manufactured by steel manufacturers is subjected to finish hot-rolling at a finishing temperature not lower than the Ar3 transformation point thereof, then washed with acid and cold-rolled into a sheet having a predetermined thickness. Next, this is degreased, then subjected to decarburizing annealing in a wet atmosphere in a box-type annealing furnace, and optionally subjected to secondary cold-rolling to a reduction ratio of at least 50 % so as to make it have a thickness of final products.

- 15   **[0003]** The cold-rolled sheet steel produced according to this process is photo-etched by etching workers, and then annealed for softening it and thereafter pressed to make it have a predetermined shape by pressing workers. Next, this is annealed in an oxidizing atmosphere for forming an oxide film, or that is, a so-called blackened film on its surface to thereby prevent it from rusting and to reduce its radiation ratio. One important characteristic that the sheet steel is desired to have is soft magnetism. Along with the inner shield therein, the shadow mask in TV Braun tubes acts to protect the linear motion of electron beams from the external magnetic field in the environment such as geomagnetism (this is hereinafter referred to as environmental magnetic field), and therefore it must be readily magnetized by itself in the environmental magnetic field. In addition, when the direction of TV is changed, the shadow mask is magnetized in the same direction in accordance with the environmental magnetic field, and therefore, it is desirable that the demagnetizability of the shadow mask is good. To satisfy the desired soft magnetic characteristics, it is desirable that the shadow mask material has a small value of coercive force (hereinafter this is simply referred to as Hc).

- 20   **[0004]** For reducing the coercive force of the shadow mask material, it is desirable to coarsen the crystal grains of the material. However, coarsening the crystal grains of the conventional shadow mask material is limited, and Hc of the material is from 103 to 135 A/m or so though depending on the annealing temperature thereof. The material does not satisfy the above-mentioned requirements.

- 25   **[0005]** Given that situation, an object of the present invention is to provide a shadow mask material which is superior to the conventional shadow mask material in point of the soft magnetism, especially having a remarkably lowered Hc to satisfy the ultra-soft magnetism necessary for shadow masks, and to provide a method for producing the material, a shadow mask and a picture tube.

- 30   **[0006]** The material for shadow masks of the invention that solves the above-mentioned problems is characterized in that it contains N  $\leq$  0.0030 % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities and it forms a shadow mask having a coercive force of at most 90 A/m.

- 35   **[0007]** More preferably, the material for shadow masks of the invention contains C  $\leq$  0.0030 % by weight, Si  $\leq$  0.03 % by weight, Mn of from 0.1 to 0.5 % by weight, P  $\leq$  0.02 % by weight, S  $\leq$  0.02 % by weight, Al of from 0.01 to 0.07 % by weight, N  $\leq$  0.0030 % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities and it forms a shadow mask having a coercive force of at most 90 A/m.

- 40   **[0008]** One method for producing the material for shadow masks of the invention is characterized in that a steel ingot that contains N  $\leq$  0.0030 % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities is hot-rolled at a finishing temperature lower than the Ar3 point thereof by from 0 to 30°C, coiled at a coiling temperature of from 540 to 700°C, washed with acid, cold-rolled and then continuously annealed to make it have a remaining C amount of at most 0.0015 % by weight.

- 45   **[0009]** Another method for producing the material for shadow masks of the invention that solves the above-mentioned problems is characterized in that a steel ingot that contains C  $\leq$  0.0030 % by weight, Si  $\leq$  0.03 % by weight, Mn of from 0.1 to 0.5 % by weight, P  $\leq$  0.02 % by weight, S  $\leq$  0.02 % by weight, Al of from 0.01 to 0.07 % by weight, N  $\leq$  0.0030 % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities is hot-rolled at a finishing temperature lower than the Ar3 point thereof by from 0 to 30°C, coiled at a coiling temperature of from 540 to 700°C, pickled, cold-rolled, and then continuously annealed to make it have a remaining C amount of at most 0.0015 % by weight, and thereafter subjected to secondary rolling to a reduction ratio of from 30 to 45 %.

- 50   **[0010]** The shadow mask of the invention is characterized in that it uses the above-mentioned shadow mask and is an ultra-thin shadow mask having a coercive force of at most 90 A/m and a thickness of from 0.05 to 0.25 mm; and

the picture tube of the invention is characterized in that it comprises the above-mentioned shadow mask.

#### BEST MODES OF CARRYING OUT THE INVENTION

5 [0011] Preferably, the hot-rolled sheet steel to be the material for shadow masks in the embodiments of the invention is formed of a steel ingot that contains  $N \leq 0.003$  % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities, and has a coercive force of at most 90 A/m.

[0012] The reasons for numerical limitations of the components are mentioned below.

Nitrogen N:  $N \leq 0.0030$  % by weight.

10 [0013] N in steel forms a nitride with Al and reduces solid solution of N, therefore reducing the aging resistance of steel. Accordingly, it is desirable that the amount of N in steel is as small as possible. For ensuring the pressability of the material for shadow masks, the amount of N must be as small as possible. Therefore, it is desirable that the uppermost limit of N is 0.0030 % by weight. More preferably, it is at most 0.0020 % by weight.  
Boron B:  $0.5 \leq B/N \leq 2$ , more preferably  $0.8 \leq B/N \leq 1.2$ .

15 [0014] B in steel acts to coarsen the crystal grains in thin sheet steel, and is therefore effective for making steel have good magnetic characteristics favorable for shadow mask materials. Especially in ultra-thin shadow masks having a thickness of from 0.08 mm to 0.25 mm or so that are used these days, the effect of B is remarkable. In addition, since B in steel is effective for fixing solid solution of N, it is desirable to add B to steel for use in the invention. On the other hand, however, too much B will fine down the crystal grains of steel and will detract from the magnetic characteristics of steel. Therefore, it is desirable that the B content of steel is defined to fall within a predetermined range. From that viewpoint, the amount of B is preferably so selected in relation to N that it satisfies  $0.5 \leq B/N \leq 2$ , more preferably  $0.8 \leq B/N \leq 1.2$ .

Coercive force Hc:  $Hc \leq 90$  A/m.

20 [0015] In order to obtain shadow masks of better demagnetizability than conventional shadow masks having a coercive force of from 103 to 135 A/m, it is desirable that the coercive force of the material for shadow masks is at most 90 A/m.

[0016] Further in the invention, it is desirable to use a steel ingot having the composition mentioned below for the material of hot-rolled sheet steel. The steel ingot of the type is preferred for the material of ultra-thin shadow masks which are used these days and have a thickness of from 0.08 mm to 0.25 mm or so.

25 [0017] Specifically, the composition of the steel ingot contains  $C \leq 0.0030$  % by weight,  $Si \leq 0.03$  % by weight, Mn of from 0.1 to 0.5 % by weight,  $P \leq 0.02$  % by weight,  $S \leq 0.02$  % by weight, and Al of from 0.01 to 0.07 % by weight. The reasons for the numerical limitation of the individual components are mentioned below.

Carbon C:  $C \leq 0.0030$  % by weight.

30 [0018] The amount of C in hot-rolled sheet steel has a significant influence on the continuous annealing process of decarburizing the steel. If it is higher than 0.0030 % by weight, then the steel could not be well decarburized in the process of continuously annealing it. If so, the annealing temperature must be elevated and the annealing time must be prolonged in order that the remaining C content of the shadow mask material could be at most 0.0015 % by weight, preferably at most 0.0008 % by weight, and it increases the production costs and lower the productivity. Accordingly, it is desirable that the uppermost limit of the C content is 0.0030 % by weight. Preferably, the C content is at most 0.0025 % by weight, more preferably at most 0.0020 % by weight.

Silicon Si:  $Si \leq 0.03$  % by weight.

35 [0019] Si in the shadow mask material is an element that is against the blackening operation in fabricating picture tubes, and its amount is preferably as small as possible. However, Si is an inevitable element in Al killed steel, and it is desirable that its uppermost limit is 0.03 % by weight. Preferably, it is at most 0.025 % by weight, more preferably at most 0.02 % by weight.

Manganese Mn: from 0.1 to 0.5 % by weight.

40 [0020] Mn in hot-rolled sheet steel is a component that is necessary for preventing the steel from undergoing red shortness by an impurity S during hot rolling. Therefore, since the material for ultra-thin shadow masks to which the invention is directed is often cracked during cold rolling, it is desirable that a predetermined amount of Mn is positively added to it. For the effect, the amount of the element is preferably at least 0.1 % by weight, more preferably at least 0.25 % by weight. However, if its amount is over 0.6 %, the component will worsen the shapability of steel. Therefore, its amount is preferably at most 0.5 % by weight, more preferably at most 0.40 % by weight, even more preferably at most 0.35 % by weight. Phosphorus P  $\leq 0.02$  % by weight.

45 [0021] P in the shadow mask material acts to fine down the crystal grains therein and therefore worsens the magnetic characteristics of the material. Accordingly, its amount is preferably as small as possible. In particular, the influence of P on the material for ultra-thin shadow masks of the invention is significant. Therefore, P is preferably at most 0.02 % by weight.

Sulfur S  $\leq 0.02$  % by weight.

**[0022]** S in hot-rolled sheet steel is an inevitable element, and it is an impurity that causes red shortness during hot rolling. Its amount is preferably as small as possible. Since the material for ultra-thin shadow masks of the invention is often cracked during cold rolling, it is desirable to positively remove S from it. To that effect, the amount of S is preferably at most 0.02 % by weight, more preferably at most 0.01 % by weight.

Aluminum Al: from 0.01 to 0.07 % by weight.

**[0023]** Al in hot-rolled sheet steel is one that is added to steel bath as a deoxidizing agent and is removed from it as slag. However, if its amount is too small, it could not exhibit stable deoxidation. To that effect, its amount is preferably at least 0.01 % by weight, more preferably at least 0.02 % by weight. However, even if its amount is over 0.07 % by weight, its effect could no more increase. Since the crystal grains of steel for use in the invention are preferably coarse, it is undesirable to add too much Al to steel since it will fine down the crystal grains. Therefore, the amount of Al is preferably at most 0.07 % by weight, more preferably at most 0.04 % by weight.

Balance: Fe and inevitable impurities.

**[0024]** Fe, and inevitable elements that are in the material not detracting from the etchability and the pressability of the material are not limited.

**[0025]** Next described is the method for producing the material for ultra-thin shadow masks of the invention. Regarding the condition of heating the slab, if the heating temperature of the slab is lower than 1100°C, the hot rollability of the slab is not good. For surely hot-rolling the slab, it is desirable that the heating temperature is higher than 1100°C. On the other hand, if the slab-heating temperature is too high, AlN in the slab will completely dissolve and will form fine crystal grains in the hot-rolled sheet steel, and the magnetic characteristics of the sheet steel will be bad. Specifically, Hc of the sheet steel increases. Accordingly, it is desirable that the slab-heating temperature is not higher than 1250°C.

**[0026]** If the finishing temperature in hot rolling is higher than the Ar3 point of the steel, the steel will undergo  $\gamma \rightarrow \alpha$  transformation after finish rolling. Therefore, fine crystal grains will be formed in the finished steel to worsen the magnetic characteristics of the steel. Specifically, Hc of the steel increases. Accordingly, the  $\gamma \rightarrow \alpha$  transformation shall be finished before finish rolling, or that is, the  $\gamma \rightarrow \alpha$  transformation shall not occur after finish rolling to coiling up. Therefore, the finishing temperature in hot rolling is lower than the Ar3 point of the steel by from 0 to 30 °C, preferably by from 10 to 20°C. The coiling temperature preferably falls between 540 and 700°C in view of the quality stability in the coil width direction and the machine direction in hot rolling, but more preferably between 650 and 700°C for enlarging the crystal grains in the hot-rolled sheet steel. The uppermost limit of the coiling temperature is not limited from the magnetic characteristics of the steel, but is 700°C from the scale removability in the step of washing the steel with acid. The lowermost limit of the temperature is 540°C or higher in view of the Hc of the steel.

(Steps of pickling, primary and secondary cold rolling)

**[0027]** Pickling and primary cold rolling may be effected under ordinary conditions. For efficiently decarburizing and annealing the ultra-thin shadow mask material of the invention, it is desirable that the thickness of the primary cold-rolled sheet steel is at most 0.6 mm. For reducing the Hc of the sheet steel, the secondary rolling reduction shall be from 30 to 45 %. The lowermost limit of the secondary rolling reduction is not specifically defined from the magnetic characteristics of the sheet steel, but shall be at least 30 % in view of the mechanical characteristics of the sheet steel products. Concretely, users of the products desire that the tensile strength of the sheet steel is at least 500 MPa. To satisfy it, the secondary rolling reduction in producing the sheet steel is at least 30 %. The thickness of the primary-rolled sheet steel will be at least 0.42 mm, preferably at least 0.38 mm, considering that the product thickness is from 0.08 to 0.25 mm.

(Continuous annealing step)

**[0028]** Continuous annealing is an important step in the invention where steel is subjected to decarburizing annealing. For the continuous annealing, preferably, the sheet temperature is not lower than 750°C, the soaking time is 60 seconds or longer, the annealing atmosphere comprises from 0 to 75 % by weight of hydrogen gas with a balance of nitrogen gas, and the dew point is from -30 to 70°C.

(Annealing temperature)

**[0029]** The annealing temperature has a significant influence on the decarburization efficiency and the magnetic characteristics of the processed steel. If it is lower than 750°C, the decarburization will take a lot of time and the productivity will be poor, and, in addition, the recrystallized texture of the annealed steel is uneven and the steel could not have uniform magnetic characteristics. Accordingly, the annealing temperature is preferably not lower than 750°C, more preferably not lower than 800°C. The uppermost limit of the annealing temperature may be 850°C in view of the

durability of the apparatus.

(Annealing time)

5 [0030] Preferably, the annealing time is not shorter than 60 seconds. If it is shorter than 60 seconds, the sheet steel could not be satisfactorily decarburized enough for the material for ultra-thin shadow masks, and it will be difficult to make the material have the intended C content of not larger than 0.0015 %. It is unnecessary to specifically define the uppermost limit of the annealing time, but the time is preferably not longer than 180 seconds in view of the productivity and for preventing the formation of too coarse grains in the sheet steel. (Hydrogen concentration in continuous annealing atmosphere, and dew point)

10 [0031] When the hydrogen concentration in the continuous annealing atmosphere is kept at most 70 %, then the C content of the ultra-thin shadow mask material could be at most 0.0015 %. Even if the hydrogen concentration therein is higher than 70 %, it could not have any influence on the decarburization time, but would rather increase the production costs. Therefore, it is desirable that the uppermost limit of the hydrogen concentration is 70 %. When the dew point falls between -35 and 70°C, then the C content of the ultra-thin shadow mask material could be at most 0.0015 %.

(Secondary cold-rolling step after annealing)

20 [0032] It is a matter of importance that the rolling reduction in the secondary cold rolling step after the annealing is from 30 to 45 % in order that the Hc of the sheet steel could be at most 90 A/m. If the rolling reduction is smaller than 30 %, the tensile strength, one mechanical property of the sheet steel will be smaller than 500 MPa and the mechanical strength of the steel will be poor; but if larger than 45 %, the Hc of the steel will increase.

#### EXAMPLES

25 [0033] The invention is described in more detail with reference to the following Examples. The steel ingots having the chemical compositions of Example 1 to Example 5 shown in Table 1 were hot rolled under the condition shown in Table 2 into hot-rolled sheet steel of 2.3 mm thick. These were pickled and then cold-rolled into sheets having a thickness of 0.3 mm. Next, these were continuously annealed under the condition shown in Table 2 for decarburization. The annealing temperature was 800°C. The process gave shadow mask materials of Examples 1 to 5. Similarly but for comparison, the steel ingots having the chemical compositions of Comparative Examples 1 to 6 in Table 1 were hot-rolled and annealed under the conditions shown in Table 2 to prepare sheet steel samples of Comparative Examples 1 to 6. Further, these were cold-rolled into ultra-thin shadow mask materials having a thickness of 0.25 mm.

30 [0034] The mechanical characteristic and the magnetic characteristic of the shadow mask materials of Examples and Comparative Examples obtained in the manner as above were measured to evaluate the materials. The results are given in Table 3.

35 [0035] For the mechanical characteristic, the tensile strength (abbreviated as T.S.) of JIS #5 sample pieces of each material was measured. In Table 3, O indicates the material having a tensile strength of at least 500 MPa, and X indicates the material having a tensile strength of lower than 500 MPa.

40 [0036] Next, the magnetic characteristic of the shadow mask materials obtained herein was evaluated as follows: The shadow mask materials were again annealed, and the Hc thereof, one important parameter of magnetic characteristics was measured in the manner mentioned below to evaluate the magnetic characteristic of the materials.

Table 1 Chemical Compositions of Steel Ingots

Example or Comparative Example	Chemical Composition (wt%)							B/N
	C	Si	Mn	P	S	Al	N	
Example 1	0.0022	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Example 2	0.0023	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Example 3	0.0028	0.02	0.24	0.009	0.008	0.063	0.0021	0.0031
Example 4	0.0028	0.02	0.24	0.009	0.008	0.063	0.0021	0.0031
Example 5	0.0028	0.02	0.24	0.009	0.008	0.063	0.0021	0.0031
Comp. Ex. 1	0.0022	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Comp. Ex. 2	0.0023	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Comp. Ex. 3	0.0022	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Comp. Ex. 4	0.0023	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Comp. Ex. 5	0.0022	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021
Comp. Ex. 6	0.0023	0.01	0.10	0.006	0.005	0.059	0.0030	0.0021

Table 2 Conditions in Producing Materials

Example or Comparative Example	Hot-Rolling Condition		Annealing		Secondary Rolling Reduction	C after annealing (wt%)
	Finishing Temperature (°C)	Coiling Temperature (°C)	System	Annealing Temperature		
Example 1	870	670	continuous annealing	800°C	42 %	0.0008
Example 2	860	670	continuous annealing	800°C	42 %	0.0008
Example 3	870	670	continuous annealing	800°C	42 %	0.0011
Example 4	870	670	continuous annealing	800°C	38 %	0.0011
Example 5	850	650	continuous annealing	800°C	42 %	0.0011
Comp. Ex. 1	840	670	continuous annealing	800°C	42 %	0.0008
Comp. Ex. 2	900	670	continuous annealing	800°C	42 %	0.0008
Comp. Ex. 3	860	500	continuous annealing	800°C	42 %	0.0008
Comp. Ex. 4	860	670	continuous annealing	800°C	25 %	0.0008
Comp. Ex. 5	870	670	continuous annealing	800°C	60 %	0.0008
Comp. Ex. 6	870	710	continuous annealing	800°C	42 %	0.0008

[0037] The annealing condition was as follows: The sheet steel was annealed at two different temperatures, 725°C and 830°C each for 10 minutes. The atmosphere was comprised of 5.5 % by weight of hydrogen with a balance of nitrogen gas. The dew point was 10°C. Hc of each sample sheet was obtained according to a tetrode Epstein's method. In Table 3, O indicates the sample having a magnetic characteristic Hc of smaller than 90 A/m; and × indicates the sample having Hc of 90 A/m or more. The descalability was evaluated as follows: The samples were dipped in a 30 wt.% H<sub>2</sub>SO<sub>4</sub> solution for 30 seconds, and visually checked for scale. × indicates the sample with scale; and O indicates the sample with no scale.

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Table 3 Results of Characteristic Evaluation

Example or Comparative Example	Mechanical Characteristic (T.S.) (MPa)	Magnetic Characteristic		Evaluation		
		725°C	830°C	Mechanical Characteristic (T.S.)	Magnetic Characteristic (Hc)	Descalability
		Hc (A/m)	Hc (A/m)			
Example 1	530	85	83	0	0	0
Example 2	532	86	84	0	0	0
Example 3	541	87	88	0	0	0
Example 4	542	88	87	0	0	0
Example 5	509	82	82	0	0	0
Comp. Ex. 1	533	94	94	0	x	0
Comp. Ex. 2	540	92	90	0	x	0
Comp. Ex. 3	560	94	93	0	x	0
Comp. Ex. 4	420	78	78	x	0	0
Comp. Ex. 5	610	95	94	0	x	0
Comp. Ex. 6	520	83	82	0	0	x

[0038] The results in Table 3 obviously confirm that the materials of Examples 1 to 5 all have a coercive force  $H_c$ , one parameter of magnetic characteristics, of lower than 90 A/m under any temperature condition of 725 and 830°C and their magnetic characteristics are favorable for shadow mask materials. In addition, it is understood that, when the pre-annealing temperature is elevated from 725°C to 830°C, then the crystals grow into large crystal grains in the products and the magnetic characteristic ( $H_c$ ) is thereby improved. The results further confirm the excellent mechanical characteristic and descalability of the materials of the invention. As opposed to these,  $H_c$  of the comparative materials is 90 A/m or more except in Comparative Example 4 and Comparative Example 6, and the comparative materials do not have the desired ultra-soft magnetic characteristic. The materials of Examples 1 and 2 of the invention are better than the materials of Comparative Examples 1 and 2 in point of the magnetic characteristic. The reason is because of the influence of the finishing temperature in rolling on the rolled sheets. In addition, they are better than the material of Comparative Example 3 also in point of the magnetic characteristic. The reason is because of the influence of the take-up temperature on the coiled sheets. The magnetic characteristic of the material of Comparative Example 4 is good, but the mechanical characteristic thereof is lower than 500 MPa. This means that users will be difficult to handle it. The materials of Examples 1 and 2 of the invention are better than the material of Comparative Example 5 in point of the magnetic characteristic ( $H_c$ ). This is because of the influence of the secondary rolling reduction on the rolled sheets. The characteristics of the material of Comparative Example 6 are good, but the coiling temperature for it is high and, in addition, its descalability is not good. Therefore, this is unfavorable for industrial-scale production.

#### INDUSTRIAL APPLICABILITY

[0039] As described hereinabove, the present invention provides a shadow mask material which has better soft magnetic characteristics than conventional shadow mask materials, especially having a significantly lowered coercive force  $H_c$  and satisfying the soft magnetism necessary for shadow masks. In particular, the mechanical characteristics (tensile strength) of the material of the invention are good and the ultra-soft magnetic characteristics thereof are also good, and the material is favorable for ultra-thin shadow masks. The invention also provides shadow masks formed of the material, and picture tubes that comprise the shadow mask.

#### Claims

1. A material for shadow masks, which is **characterized in that** it contains  $N \leq 0.0030$  % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities and it forms a shadow mask having a coercive force of at most 90 A/m.
2. A material for shadow masks, which is **characterized in that** it contains  $C \leq 0.0030$  % by weight,  $Si \leq 0.03$  % by weight, Mn of from 0.1 to 0.5 % by weight,  $P \leq 0.02$  % by weight,  $S \leq 0.02$  % by weight, Al of from 0.01 to 0.07 % by weight,  $N \leq 0.0030$  % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities and it forms a shadow mask having a coercive force of at most 90 A/m.
3. A method for producing a material for shadow masks, which is **characterized in that** a steel ingot that contains  $N \leq 0.0030$  % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities is hot-rolled at a finishing temperature lower than the  $Ar_3$  point thereof by from 0 to 30°C, coiled at a take-up temperature of from 540 to 700°C, washed with acid, cold-rolled and then continuously annealed to make it have a remaining C amount of at most 0.0015 % by weight.
4. A method for producing a material for shadow masks, which is **characterized in that** a steel ingot that contains  $C \leq 0.0030$  % by weight,  $Si \leq 0.03$  % by weight, Mn of from 0.1 to 0.5 % by weight,  $P \leq 0.02$  % by weight,  $S \leq 0.02$  % by weight, Al of from 0.01 to 0.07 % by weight,  $N \leq 0.0030$  % by weight and B to satisfy  $0.5 \leq B/N \leq 2$  with a balance of Fe and inevitable impurities is hot-rolled at a finishing temperature lower than the  $Ar_3$  point thereof by from 0 to 30°C, coiled at a take-up temperature of from 540 to 700°C, washed with acid, cold-rolled, and then continuously annealed to make it have a remaining C amount of at most 0.0015 % by weight, and thereafter subjected to secondary rolling to a reduction ratio of from 30 to 45 %.
5. A shadow mask formed of the material of claim 1 or 2, which has a coercive force of at most 90 A/m and a thickness of from 0.05 to 0.25 mm.
6. A picture tube that comprises the shadow mask of claim 5.

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP01/09964

## A. CLASSIFICATION OF SUBJECT MATTER

Int.Cl.<sup>7</sup> C22C 38/00, H01J 29/07, H01J 9/14

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Int.Cl.<sup>7</sup> C22C 38/00, H01J 29/07, H01J 9/14

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Jitsuyo Shinan Koho	1926-1996	Jitsuyo Shinan Toroku Koho	1996-2002
Kokai Jitsuyo Shinan Koho	1971-2002	Toroku Jitsuyo Shinan Koho	1994-2002

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP 11-323500 A (NKK Corporation),	1-2, 5-6
Y	26 November, 1999 (26.11.1999), working example (Family: none)	4
X	JP 55-138027 A (NKK Corporation),	3
Y	28 October, 1980 (28.10.1980), working example (Family: none)	4

☐ Further documents are listed in the continuation of Box C.☐ See patent family annex.

\* Special categories of cited documents:

"A" document defining the general state of the art which is not

considered to be of particular relevance

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date

"L" document which may throw doubts on priority claim(s) or which is

cited to establish the publication date of another citation or other

special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other

means

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than the priority date claimed

"I" later document published after the international filing date or

priority date and not in conflict with the application but cited to

understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be

considered novel or cannot be considered to involve an inventive

step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be

considered to involve an inventive step when the document is

combined with one or more other such documents, such

combination being obvious to a person skilled in the art

"&amp;" document member of the same patent family

Date of the actual completion of the international search

05 February, 2002 (05.02.02)

Date of mailing of the international search report

12 February, 2002 (12.02.02)

Name and mailing address of the ISA/  
Japanese Patent Office

Authorized officer

Facsimile No.

Telephone No.

Form PCT/ISA/210 (second sheet) (July 1992)

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 01/42675

A. CLASSIFICATION OF SUBJECT MATTER  
 IPC 7 H01M12/02 H01M2/34

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 H01M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

PAJ, EPO-Internal

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	PATENT ABSTRACTS OF JAPAN vol. 013, no. 150 (E-742), 12 April 1989 (1989-04-12) & JP 63 310577 A (MATSUSHITA ELECTRIC IND CO LTD), 19 December 1988 (1988-12-19)	1,13
Y	abstract	2-8, 15-21
Y	WO 95 06691 A (BRIES JAMES L ;HAMERSKI MICHAEL D (US); MINNESOTA MINING & MFG (US) 9 March 1995 (1995-03-09) page 2, line 3 -page 3, line 29 page 5, line 11 -page 7, line 21 page 11, line 1-16; claims 1-17	2-8, 15-21
X	US 5 191 274 A (LLOYD ROBERT D ET AL) 2 March 1993 (1993-03-02) column 2, line 4-44; claims 1-12	1,13
-/-		

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

## \* Special categories of cited documents:

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\*P\* document published prior to the international filing date but later than the priority date claimed

\*T\* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

\*X\* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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\*Z\* document member of the same patent family

Date of the actual completion of the international search

11 February 2003

Date of mailing of the international search report

18/02/2003

Name and mailing address of the ISA

European Patent Office, P.B. 5816 Patentlaan 2  
 NL - 2280 HV Rijswijk  
 Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
 Fax: (+31-70) 340-3016

Authorized officer

De Vos, L

## INTERNATIONAL SEARCH REPORT

 International Application No  
 PCT/US 01/42675

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	PATENT ABSTRACTS OF JAPAN vol. 013, no. 016 (E-703), 13 January 1989 (1989-01-13) & JP 63 224161 A (TOSHIBA BATTERY CO LTD), 19 September 1988 (1988-09-19) abstract ---	1, 13
A	US 4 649 090 A (CARPENTER DENIS D ET AL) 10 March 1987 (1987-03-10) column 3, line 32 -column 5, line 22; claims 1-12 ---	1-25
A	PATENT ABSTRACTS OF JAPAN vol. 017, no. 480 (E-1425), 31 August 1993 (1993-08-31) & JP 05 121057 A (MATSUSHITA ELECTRIC IND CO LTD), 18 May 1993 (1993-05-18) abstract ---	1-25
A	PATENT ABSTRACTS OF JAPAN vol. 017, no. 091 (E-1324), 23 February 1993 (1993-02-23) & JP 04 284377 A (MATSUSHITA ELECTRIC IND CO LTD), 8 October 1992 (1992-10-08) abstract ---	1-25
A	EP 0 845 514 A (BEIERSDORF AG) 3 June 1998 (1998-06-03) page 2, line 34 -page 3, line 52; claims 1-10 -----	1-12

Form PCT/ISA/210 (continuation of second sheet) (July 1992)

## INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 01/42675

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
JP 63310577	A	19-12-1988	NONE
WO 9506691	A	09-03-1995	AU 685159 B2 15-01-1998
		AU 7676494 A 22-03-1995	
		CA 2168370 A1 09-03-1995	
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US 5191274	A	02-03-1993	NONE
JP 63224161	A	19-09-1988	JP 2585250 B2 26-02-1997
US 4649090	A	10-03-1987	DE 3681720 D1 31-10-1991
		DK 614786 A 23-07-1987	
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EP 0845514	A	03-06-1998	DE 19649727 A1 04-06-1998
		EP 0845514 A2 03-06-1998	
		US 5897949 A 27-04-1999	

## INTERNATIONAL SEARCH REPORT

(PCT Article 18 and Rules 43 and 44)

Applicant's or agent's file reference <b>M-4928</b>	<b>FOR FURTHER ACTION</b> see Notification of Transmittal of International Search Report (Form PCT/ISA/220) as well as, where applicable, item 5 below.	
International application No. <b>PCT/US 01/ 42675</b>	International filing date (day/month/year) <b>12/10/2001</b>	(Earliest) Priority Date (day/month/year) <b>19/10/2000</b>
Applicant <b>THE GILLETTE COMPANY</b>		

This International Search Report has been prepared by this International Searching Authority and is transmitted to the applicant according to Article 18. A copy is being transmitted to the International Bureau.

This International Search Report consists of a total of 4 sheets.  
☒ It is also accompanied by a copy of each prior art document cited in this report.

**1. Basis of the report**

a. With regard to the language, the international search was carried out on the basis of the international application in the language in which it was filed, unless otherwise indicated under this item.

☐ the international search was carried out on the basis of a translation of the international application furnished to this Authority (Rule 23.1(b)).

b. With regard to any nucleotide and/or amino acid sequence disclosed in the international application, the international search was carried out on the basis of the sequence listing:

☐ contained in the international application in written form.

☐ filed together with the international application in computer readable form.

☐ furnished subsequently to this Authority in written form.

☐ furnished subsequently to this Authority in computer readable form.

☐ the statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.

☐ the statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

2. ☐ Certain claims were found unsearchable (See Box I).

3. ☐ Unity of Invention is lacking (see Box II).

4. With regard to the title,

☒ the text is approved as submitted by the applicant.

☐ the text has been established by this Authority to read as follows:

5. With regard to the abstract,

☒ the text is approved as submitted by the applicant.

☐ the text has been established, according to Rule 38.2(b), by this Authority as it appears in Box III. The applicant may, within one month from the date of mailing of this international search report, submit comments to this Authority.

6. The figure of the drawings to be published with the abstract is Figure No. 1

☒ as suggested by the applicant.

☐ because the applicant failed to suggest a figure.

☐ because this figure better characterizes the invention.

☐ None of the figures.

Form PCT/ISA/210 (first sheet) (July 1998)

From the INTERNATIONAL SEARCHING AUTHORITY

**PCT**NOTIFICATION OF TRANSMITTAL OF  
THE INTERNATIONAL SEARCH REPORT  
OR THE DECLARATION

(PCT Rule 44.1)

To:

Ladas & Parry  
Attn. Handelman, Joseph H.  
26 West 61st Street  
New York, NY 10023-7604  
UNITED STATES OF AMERICADate of mailing  
(day/month/year)

18/02/2003

Applicant's or agent's file reference

M-4928

**FOR FURTHER ACTION**

See paragraphs 1 and 4 below

International application No.

PCT/US 01/42675

International filing date

(day/month/year)

12/10/2001

Applicant

THE GILLETTE COMPANY

- 1.
- ☒
- The applicant is hereby notified that the International Search Report has been established and is transmitted herewith.

**Filing of amendments and statement under Article 19:**

The applicant is entitled, if he so wishes, to amend the claims of the International Application (see Rule 45):

**When?** The time limit for filing such amendments is normally 2 months from the date of transmittal of the International Search Report; however, for more details, see the notes on the accompanying sheet.**Where?** Directly to the International Bureau of WIPO  
34, chemin des Colombettes  
1211 Geneva 20, Switzerland  
Facsimile No.: (41-22) 740.14.35

For more detailed instructions, see the notes on the accompanying sheet.

- 2.
- ☐
- The applicant is hereby notified that no International Search Report will be established and that the declaration under Article 17(2)(e) to that effect is transmitted herewith.

- 3.
- ☐
- With regard to the protest against payment of (an) additional fee(s) under Rule 40.2, the applicant is notified that:

☐ the protest together with the decision thereon has been transmitted to the International Bureau together with the applicant's request to forward the texts of both the protest and the decision thereon to the designated Offices.☐ no decision has been made yet on the protest; the applicant will be notified as soon as a decision is made.

- 4.
- Further action(s):**
- The applicant is reminded of the following:

Shortly after 18 months from the priority date, the international application will be published by the International Bureau. If the applicant wishes to avoid or postpone publication, a notice of withdrawal of the international application, or of the priority claim, must reach the International Bureau as provided in Rules 90bis.1 and 90bis.3, respectively, before the completion of the technical preparations for international publication.

Within 19 months from the priority date, a demand for international preliminary examination must be filed if the applicant wishes to postpone the entry into the national phase until 30 months from the priority date (in some Offices even later).

Within 20 months from the priority date, the applicant must perform the prescribed acts for entry into the national phase before all designated Offices which have not been elected in the demand or in a later election within 19 months from the priority date or could not be elected because they are not bound by Chapter II.

Name and mailing address of the International Searching Authority

European Patent Office, P.B. 5818 Patentlaan 2  
NL-2280 HV Rijswijk  
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
Fax: (+31-70) 340-3016

Authorized officer

Maria Van der Hoeven

Form PCT/ISA/220 (July 1998)

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